บันทึกข้อความ

สำนักงาน หน่วยนิเทศสุขภาพประจวบคีรีขันธ์ มหาวิทยาลัยอุบลราชธานี โทร.3319
ที่ ศก 0529.8.4 / 1616 วันที่ 5 พฤศจิกายน 2560
เรื่อง ขออนุมัติเบิกงบประมาณเพื่อเข้าเสีย脱落ระบบวิจัยในการประชุมวิชาการระดับนานาชาติในประเทศ

เรียน รองอธิบดีฝ่ายวิจัยและบริการวิชาการ สำนักงานมหาวิทยาลัยศรีนครินทรวิโรฒ

ตามที่ผ่านมา ดร.คมสันต์ ขันกิจสุรนารี คณบดีฝ่ายวิจัย ประชุมวิชาการระดับประเทศ ได้รับการตอบรับในการเข้าเสีย脱落ระบบวิจัย เรื่อง Mass Diffusion Coefficient Measurement for Vitreous Humor Using FEM and MRI ในการประชุมวิชาการระดับนานาชาติ The 8th TSME International Conference on Mechanical Engineering ระหว่างวันที่ 12 – 15 ธันวาคม 2560 ณ ประเทศไทย นั้น

ดังนั้น เพื่อให้การเข้าเสีย脱落ระบบวิจัยเป็นไปด้วยความเรียบร้อย จึงขออนุมัติเบิกงบประมาณ เพื่อการเข้าเสีย脱落ระบบวิจัยดังกล่าว เป็นจำนวนเงิน 15,560 บาท (หนึ่งหมื่นห้าพันห้าร้อยหกสิบบาทถ้วน) โดยมีรายละเอียดในรายการเบิกจ่ายดังนี้

1. ค่าลงทะเบียน 10,500 บาท
2. ค่าพาหนะภายในประเทศ (ไป-กลับ: อุบลฯ-กรุงเทพฯ) 2,500 บาท
3. ค่าโดยสารประจำทาง 1,600 บาท
4. ค่าเบี้ยพำนักในประเทศ (240 บาท × 4 วัน) 960 บาท

ทั้งนี้ ขอขอบคุณสำนักงานด้วยที่รับรอง ไม่เป็นส่วนหนึ่งของคุณสมบัติของบุคคลที่มีการจัดสรร และขออนุมัติเบิกงบประมาณตามที่ขอร้องจึงยินดี ขอรับเงิน 15,560 บาท (หนึ่งหมื่นห้าพันห้าร้อยหกสิบบาทถ้วน)

จึงเรียนมาเพื่อโปรดพิจารณา

(นายจิต โพธิ์งาม)

(ดร.คมสันต์ ขันกิจสุรนารี)

หัวหน้าบริการวิชาการ สำนักงานมหาวิทยาลัยศรีนครินทรวิโรฒ

อาจารย์ประจำมหาวิทยาลัยศรีนครินทรวิโรฒ
The 8th TSME International Conference on Mechanical Engineering
12-15 December 2017, Bangkok

Early-bird Registration Form

Participant Name: Komsan Ratanakijisuntorn

Paper ID (Leave blank for non-speaker): ICOME-2017-0279

Paper Title (Leave blank for non-speaker): Mass Diffusion Coefficient Measurement for Vitreous Humor Using FEM and MRI

University/Organization: Ubon Ratchathani University

Billing Address: Faculty of Engineering, Department of Mechanical Engineering, Ubon Ratchathani University, 85 Sathonlamark Road, Warinchamrap, Ubon Ratchathani 34190

Phone: 092-684-5885 E-mail: komsan.r@ubu.ac.th

Special Events
✓ I will join the banquet dinner on a cruise on 14 December 2017.
✓ I will join the excursion trip in the afternoon of 15 December 2017.

Attendance Category

Please select only one category:

<table>
<thead>
<tr>
<th>Category</th>
<th>Registration fee (THB)</th>
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<tr>
<td>Speaker (General) + Regular ICOME2017 Proceedings</td>
<td>7,500.-</td>
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<tr>
<td>Speaker (General) + IOP Conference Series Proceedings</td>
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Additionally, I have ___ guest(s)/spouse who are also attending the conference. The additional fee is 2,000 THB per guest/spouse. Please add this additional fee to the base amount above.

Guest Name(s): ..............................................................

Total amount payable: 10,500.-

( Total amount payable = Registration fee + Number of guests x 2,000 THB )

Please fill out this form and email it with a proof of payment to icome2017.register@eng.kmutnb.ac.th

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  (Thomson Reuters Web of Science)
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- Compendex
- Inspec
- INS (International Nuclear Information System)
- Chemical Abstracts
- NASA Astrophysics Data System
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<th>Session</th>
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<tr>
<td>13 December</td>
<td>Registration @ 2nd Floor Foyer</td>
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<td>13:00 - 18:00</td>
<td>Registration/Networking</td>
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<td>13 December</td>
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<tr>
<td>08:00 - 08:30</td>
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<tr>
<td>08:30 - 09:00</td>
<td>Welcome Speech by</td>
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<tr>
<td></td>
<td>Prof. Dr. Suwat Kuntanapreeda and Assoc. Prof. Dr. Sinchal Chinvorarat</td>
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<tr>
<td></td>
<td>Conference Co-Chairs</td>
</tr>
<tr>
<td></td>
<td>Department of Mechanical and Aerospace Engineering,</td>
</tr>
<tr>
<td></td>
<td>King Mongkut's University of Technology North Bangkok (KMITNB)</td>
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<tr>
<td></td>
<td>Prof. Dr. Ing. habil. Suchart Siengchin</td>
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<tr>
<td></td>
<td>President, King Mongkut's University of Technology North Bangkok (KMITNB)</td>
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<tr>
<td></td>
<td>Asst. Prof. Dr. Chinda Charoenphonphanich</td>
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<td></td>
<td>President, Thai Society of Mechanical Engineers (TSME)</td>
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<td></td>
<td>Prof. Dr. Mari Oshima</td>
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<td></td>
<td>President, The Japan Society of Mechanical Engineers (JSME)</td>
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<tr>
<td>09:00 - 09:15</td>
<td>Honorary Speaker:</td>
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<tr>
<td></td>
<td>Mr. Stefan Bienefeld</td>
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<tr>
<td></td>
<td>DAAD-Deutscher Akademischer Austauschdienst,</td>
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<td></td>
<td>German Academic Exchange Service</td>
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<tr>
<td></td>
<td>The role of DAAD support in fostering Mechanical Engineering Capacity</td>
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<td></td>
<td>for Development</td>
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<td>09:15 - 09:30</td>
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<tr>
<td></td>
<td>Dr. Eberhard Alles</td>
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<tr>
<td></td>
<td>Chancellor</td>
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<tr>
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<td>TU Chemnitz, Germany</td>
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<tr>
<td></td>
<td>Making Industry 4.0 Work: Best Practices from a University Management</td>
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<tr>
<td></td>
<td>Perspective</td>
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<td>09:30-09:55</td>
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<td></td>
<td>Univ.-Prof. Dr.-Ing. habil. Prof. E. h. Prof. Lothar Kroll</td>
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<tr>
<td></td>
<td>Director of Institute of Lightweight Structures,</td>
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<td></td>
<td>TU Chemnitz, Germany</td>
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<tr>
<td></td>
<td>Technology Fusion in Series Production of Lightweight Structures</td>
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<tr>
<td>Time</td>
<td>Session Description</td>
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| 09:55 - 10:20 | Keynote Speaker: Prof. Dr. Shinichi Nakasuka  
Department of Aeronautics and Astronautics,  
University of Tokyo, Japan  
Micro/nano/pico-satellite Challenge for Novel Space Development and Utilization |
| 10:20 - 10:40 | Coffee Break                                                                        |
| 10:40 - 11:05 | Keynote Speaker: Prof. Dr.-Ing. Helnz Peter Berg  
Chair of Combustion Engines and Flight Propulsion  
Brandenburg University of Technology Cottbus-Senftenberg, Germany  
Microturbine- and Turbo-Fuel-Cell Technology for Highly Effective Generation of Electricity -- Example of an International Technology Transfer Supported by the DAAD |
| 11:05 - 11:30 | Keynote Speaker: Prof. Dr. Yasuyuki Nishloka  
Department of Engineering and Design, Faculty of Engineering and Design  
Hosei University, Japan  
Kaizen Approach to Smart Manufacturing for Connected Industries |
| 11:30 - 11:55 | Keynote Speaker: Prof. Dr. Suwat Kuntanapreeda  
Department of Mechanical and Aerospace Engineering, Faculty of Engineering  
King Mongkut’s University of Technology North Bangkok, Thailand  
Lessons Learned from KNACKSAT Satellite |
| 11:55 - 13:00 | Lunch                                                                               |

**Session 1**

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**Session 2**

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### 14 December 2017

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**Coffee Break**

**Session 4**

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**Lunch**

**Session 5**

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Posterior Presentation (ASEAN Session)/Coffee Break

16:30 - 18:00 Move to Pier: Buses leave from the hotel parking lot

18:00 - 21:00 TSME Annual General Meeting & Banquet Dinner on a Cruise

### 15 December 2017

**Session 6**

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Coffee Break

Closing Ceremony @ Arnoma II

11:20 - 12:00 Closing Remarks and Awarding Ceremony

12:00 - 13:00 Farewell Lunch

13:00 - 16:00 Excursion Trip (Registered Participants)
Applied Mechanics, Materials and Manufacturing

AMM0001 Development of Solid State Bonding Technology for the Aluminum Alloy in Atmosphere by Using High Frequency Induction Heating and Ultrasonic Vibration
AMM0002 Application of grey-fuzzy approach in parametric optimization of EDM process in machining of MDN 300 steel
AMM0003 Fatigue Behavior of Resistance Spot Welded High Strength Steel Sheets with Different Nugget Sizes
AMM0005 Development and Comparison of Processing Maps of Mg-3Sn-1Ca Alloy from Data Obtained in Tension versus Compression
AMM0006 Compressive behavior of Sulcata Tortoise's carapace at high rate of deformation
AMM0007 Nanoindentation Tests of Sulcata Tortoise's Carapace
AMM0008 Evaluation of Tensile Strength and Consideration of the Rope Structure of Net for Super-Pressure Balloon.
AMM0009 Characteristics of Acoustic Emission from Corrosion in Anticorrosive Coated Steel
AMM0010 Development of the Novel Non-contact AE Sensor Using Air-coupled Ultrasonic Transducer for Plates and Cylinders
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Since 1987, the Thai Society of Mechanical Engineers (TSME) has been holding national conferences in Mechanical Engineering yearly. These conferences are called Mechanical Engineering Network of Thailand (ME-NETT). The objectives of the conferences are to encourage students, researchers, and interested persons to present their works, to create researching networks, to publish the research works for industry sectors, to find the needs of public and private organizations, to fulfill these demands to enhance the growth of country, and to be a hub in the field of Mechanical Engineering for anyone with an interest.

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Important Dates

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* Submission templates can be found on the Downloads page

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Mass Diffusion Coefficient Measurement for Vitreous Humor Using FEM and MRI

Komsan Rattanakijunsuntorn¹, Anita Penkova², and Satwindar S. Sadhal²

1Faculty of Engineering, Department of Mechanical Engineering, Ubon Ratchathani University, 85 Sathanlanark Road, Warinchamrap, Ubon Ratchathani 34190, Thailand
2Aerospace & Mechanical Engineering Department, University of Southern California, Los Angeles, CA 90089-1453, United States

*Corresponding Author: komsan.r@ubu.ac.th

Abstract. In early studies, the 'contour method' for determining the diffusion coefficient of the vitreous humor was developed. This technique relied on careful injection of an MRI contrast agent (surrogate drug) into the vitreous humor of fresh bovine eyes, and tracking the contours of the contrast agent in time. In addition, an analytical solution was developed for the theoretical contours built on point source model for the injected surrogate drug. The match between theoretical and experimental contours as a least square fit, while observing the diffusion coefficient, led to the value of the diffusion coefficient. This method had its limitation that the initial injection of the surrogate had to be spherical or ellipsoidal because of the analytical result based on the point-source model. With a new finite element model for the analysis in this study, the technique is much less restrictive and handles irregular shapes of the initial bolus. The fresh bovine eyes were used for drug diffusion study in the vitreous and three contrast agents of different molecular masses: gadolinium-diethylenetriaminepentaacetic acid (Gd-DTPA, 938 Da), non-ionic gadoteridol (Prohance, 559 Da), and bovine albumin conjugated with gadolinium (Galbumin, 74 kDa) were used as drug surrogates to visualize the diffusion process by MRI. The 3D finite element model was developed to determine the diffusion coefficients of these surrogates with the images from MRI. This method can be used for other types of bioporous media provided the concentration profile can be visualized (by methods such as MRI or fluorescence).

1. Introduction

During the past decades, many researchers have attempted to develop ocular drug delivery systems. Intravitreal drug delivery has become a popular method of treatment of many retinal diseases, commonly including AMD, Diabetic Retinopathy, and Retinal Vein Occlusions. While various drugs have been successfully developed, delivering drugs to the retina requires knowledge of the relevant fluid mechanics and transport phenomena. Low drug concentrations are insufficient to treat the retinal disease and high concentrations can carry risks of side effects [1-3]. Therefore, it is crucial to know the drug distribution within the eye following delivery by intravitreal injection.

With the help from the advanced computer software nowadays, ocular drug transport models have been developed to simulate and predict drug distribution in the eye [4-7]. These models require the values of parameters that are used in the governing equations, and one of the most common uses of
parameter is drug diffusivity. Therefore, the aim of this work is to develop a technique that delivers the values of diffusion coefficient of drugs in the vitreous from MRI images.

In early study by Penkova et al [8], the ‘contour method’ for determining the diffusion coefficient of the vitreous humor was developed. This technique relied on careful injection of an MRI contrast agent (surrogate drug) into the vitreous humor of fresh bovine eyes, and tracking the contours of the contrast agent in time. In addition, an analytical solution was developed for the theoretical contours built on point source model for the injected surrogate drug. The match between theoretical and experimental contours as a least square fit, while floating the diffusion coefficient, led to the value of the diffusion coefficient. This method had its limitation that the initial injection of the surrogate had to be spherical or ellipsoidal because of the analytical result based on the point-source model. With a new finite element model for the analysis in this study, the technique is much less restrictive and handles irregular shapes of the initial bolus.

2. Methods and materials

2.1. Apparatus
Whole bovine eyes were prepared for MRI visualization with the same method as described in the previous study [8]. Three gadolinium-based contrast agents: gadolinium-diethylenetriamine pentaacetic acid (Gd-DTPA, 938 Da), nonionic gadoteridol (Prohance, 559 Da), and bovine albumin conjugated with gadolinium (Galbumin, 74 kDa) were used as drug surrogates to model diffusive transport of different molecular weight drugs. Experiments were conducted by injecting 30 μL of the contrast agents in the vitreous of the whole eye. With the concentration measurement from the MRI signal at regular intervals for 2-3 hours, the concentration contours were constructed and matched with the theoretical contours from the finite element analysis. The best fit at different times gave fairly consistent values of the diffusion coefficient.

2.2. Governing equations and model development
A three-dimensional finite element model of the vitreous was developed to help in analyzing MRI images and calculate diffusion coefficients by comparing simulated data to MRI experimental data. To model the drug distribution in the vitreous, the mass transport equation was applied:

\[
\frac{\partial c}{\partial t} + \nabla \cdot (\nu c) - D \nabla^2 c + q = 0
\]  

(1)

where \( c \) represents the concentration of the drug, \( D \) is the diffusion coefficient of the drug in the vitreous, \( \nu \) is the velocity of fluid in the vitreous, and \( q \) is the release rate of the drug. Since the experiment was conducted by excluding convection in the system, and we assumed that the drug is neither generated nor degraded within the vitreous, the terms involving with \( \nu \) and \( q \) were set to zero. The mass transport equation can be rewritten as:

\[
\frac{\partial c}{\partial t} - D \nabla^2 c = 0
\]  

(2)

For the purpose of modelling, the domain of interest (of the vitreous) in which drugs diffused through was simply defined as a sphere with a radius of 10 mm as illustrated in figure 1(a). The geometry created for the domain of interest, were converted into a total of 105,276 finite element tetrahedral meshes. Since the rate of change of concentration over time near the center of the domain is larger than the outer, mesh size was varied by having finer meshes near the center and coarser meshes near the outer boundary as shown in figure 1(b).
2.3. Boundary and initial conditions
The vitreous humor in this study is considered to be a homogeneous substance. The lens is avascular and is considered to be impermeable to fluid flow, so we assumed that the drug surrogate does not penetrate the lens. Similarly, RPE is considered as a major barrier for the retinal delivery of hydrophilic drugs, the same assumption that we made for the lens also applied for the RPE. Since the outer boundary of the domain of interest reaches the regions of lens and RPE membrane, we simplified the boundary condition at the outer surface as zero flux condition. This kind of boundary condition would much simplify the finite element equation by eliminating the flux term as detailed in appendix A. The concentration distribution profiles of the MRI images were directly projected to the nodes in the finite element model as the initial condition for each time point. With this method, we can handle the situation that the concentration distribution profile was not symmetric.

2.4. Solution methodology
The concentration distribution in the vitreous was solved using the finite element method involving linear algebraic equations of the form,

$$\begin{align*}
[K_C] \left\{ \frac{dC}{dt} \right\} + D[K_D]C = 0,
\end{align*}$$

(3)

where $[K_C]$ and $[K_D]$ are the global system matrices developed from the Galerkin finite element method in appendix A. The solution employed the 3-D mesh of a total of 105,276 elements, and four nodal tetrahedral elements were used in the 3-D continuum domain. For the time discretization, we applied the well-known theta-method, which results in the equation

$$\begin{align*}
[K_C] \left\{ \frac{C^{n+1} - C^n}{\Delta t} \right\} + D[K_D](\theta C^{n+1} + (1 - \theta)C^n) = 0
\end{align*}$$

(4)

where $C^n$ is the concentration distribution at a specific time point, $C^{n+1}$ is the concentration distribution at the later time point, and the parameter $\theta$ is related to the applied numerical method. It is worth emphasizing that for $\theta = 0.5$, the method yields the Crank-Nicolson implicit method which has higher accuracy and unconditional stable for the time discretization [9]. Substituting $\theta = 0.5$ in equation (4), then it can be rewritten as,

$$\begin{align*}
([K_C] + 0.5\Delta tD[K_D])[C^{n+1}] = ([K_C] - 0.5\Delta tD[K_D])[C^n]
\end{align*}$$

(5)
In this equation, the concentration profile $C^n$ was known by projecting the concentration values of a specific time point from MRI images onto the finite element domain. The unknown parameter, $D$, was floated in order to get the calculated $C^{n+1}$ which represents the concentration at the later time step. The value of $D$ between two consecutive time points can be obtained by least square fitting of $C^{n+1}$ and the concentration profile of the later time point from MRI images.

2.5. Model validation
In order to verify the finite element diffusion model developed in the previous section, the solutions obtained from the model was compared with the exact solutions. The exact solution for a spherical bolus of radius $r_0$ in a spherical shell of radius $R$ was derived in the previous study [8] and shown in equation (6).

$$c(r, t) = c_0 \left[ \frac{r_0^3}{R^3} + 2 \sum_{n=1}^{\infty} \frac{\sin(\lambda_n r_0) - \lambda_n r_0 \cos(\lambda_n r_0)}{\lambda_n R \sin^2(\lambda_n R)} e^{-D \lambda_n^2 t} \frac{\sin(\lambda_n r)}{\lambda_n r} \right]$$  \hspace{1cm} (6)

where $c_0$ is the initial concentration of the drug deposited, $r$ is the radial distance from the point of injection, $D$ is the diffusion coefficient, $t$ is the time, $c(r, t)$ is the concentration, and $\lambda_n$ is the set of constants satisfying the transcendental equation.

$$\lambda_n R = \tan(\lambda_n R)$$  \hspace{1cm} (7)

For the model validation, we use the following parameters: $r_0 = 2$ mm, $R = 10$ mm, and $c_0 = 0.05$ in both finite element model and the exact solution, to compare the concentration values. Figure 2 shows the comparison of concentration distribution profiles from the developed model and the exact solution under the same initial and boundary conditions. The finite element solutions along the center line at a specific time ($t=40$ min) have a strong agreement with the exact solutions.

![Figure 2. The comparison of concentration distribution profiles from the finite element model and the exact solution.](image-url)
3. Results
Following the method of diffusion coefficient measurement by using MRI developed earlier, contours of constant concentration were established for different drug surrogates in each eye, and the comparison of these with the corresponding finite element calculation was shown in figure 3 where the (x, y, z) coordinate system in relation to the eye is shown in figure 4. While several time points for each eye were recorded and used in the analysis, only a selected example for each contrast agent is shown for illustrative purposes. The diffusion coefficients values of each drug surrogates acquired from the finite element method were presented in figure 5. We have made a comparison of previously reported \( D \) values for Gd-DTPA from the analytical method in the previous study [8] with the current method (finite element), and found that they were very consistent. The diffusion coefficient was \( (3.040 \pm 0.274) \times 10^{-6} \text{ cm}^2/\text{s} \) from the analytical method, and \( (3.069 \pm 0.237) \times 10^{-6} \text{ cm}^2/\text{s} \) from the finite element method. By comparing the diffusion coefficients between Gd-DTPA (molecular weight 938 Da), Prohance (molecular weight 559 Da), and Galbumin (molecular weight around 74k Da), we found that Galbumin had the lowest diffusivity, while Gd-DTPA had the highest diffusivity in the vitreous.

![Figure 3](image)

**Figure 3.** Contours of constant concentration in (A) Gd-DTPA at \( t=85 \text{ min} \), (B) Prohance at \( t=88 \text{ min} \), and (C) Galbumin at \( t=185 \text{ min} \) (---: measurement, ----: finite element).
Figure 4. Coordinate system orientation with respect to the eye. The origin located at the center of the bolus.

Figure 5. Diffusion coefficients of drug surrogates in bovine eyes.

4. Discussion
Early investigations of diffusion coefficients of different MRI contrast agents had been conducted by Gillis et al [10]. They measured diffusivity of a negatively charged contrast agent Gd-DTPA and the non-ionic gadoteridol, Prohance, in control cartilages using MRI. The diffusion coefficients for Gd-DTPA and Prohance were reported by Gillis et al as $(1.84 \pm 0.12) \times 10^{-6}$ cm$^2$/s and $(1.55 \pm 0.22) \times 10^{-6}$ cm$^2$/s respectively. In our study, we found that the diffusion coefficient in the vitreous of a smaller molecule, Prohance was $(2.739 \pm 0.340) \times 10^{-6}$ cm$^2$/s which was lower than the diffusion coefficient of
a larger molecule, Gd-DTPA. This implied that the effect of negative net charge on Gd-DTPA is likely to enhance the diffusivity in the vitreous.

Galphamin used in this experiment is a bovine albumin conjugated with gadolinium which has negative charge. Molokhia et al estimated the free aqueous diffusion coefficient of Galphamin in water at 37 °C as $8 \times 10^{-7}$ cm$^2$/s using the diffusion coefficient of bovine serum albumin (BSA), viscosity of water, and molecular weights of Galphamin and BSA [11]. The diffusion coefficient of Galphamin in this study was found to be $(2.271 \pm 0.209) \times 10^{-7}$ cm$^2$/s which is in the same order as the one estimated by Molokhia. Our lower value can also be attributed to the fact that we conducted experiments at room temperature. To compare with the smaller negative charge Gd-DTPA, Galphamin has a lower diffusion coefficient as expected.

5. Conclusion
The contour method recently developed is a very useful technique for the diffusion coefficient measurement in vitreous humor. With a new finite element model for the analysis, it can handle arbitrary shapes of the concentration contours, and we are able to show a comparison of diffusion coefficients of Gd-DTPA with Prohance and Galphamin. It has been found that both molecular weight and net charge of drugs affect the diffusion process in the vitreous humor. This method does not only work for the measurement in the vitreous humor, but also can be applied for other types of tissues in which the concentration profile can be visualized by MRI or fluorescence. The fact that we can now handle irregular shapes of the contours, the technique can be opened up to measure parameters that include convective transport effects as well.

Acknowledgement
The work in this paper is supported by NIH (National Institute of Health) under award number 5R01EY026599-02.

Appendix A. Finite element equations for the intravitreal diffusion
This section provides a detailed derivation of ‘weak form’ of the drug diffusion equation using Galerkin method. Basic concept and application of this method can be found in literature [9]. The procedure starts by considering the suitable form of the mass transport equation which is given by equation (2),

$$\frac{\partial C}{\partial t} - D \left( \frac{\partial^2 C}{\partial x^2} + \frac{\partial^2 C}{\partial y^2} + \frac{\partial^2 C}{\partial z^2} \right) = 0$$  \hspace{1cm} (A1)

![Figure A1. Linear tetrahedral element.](image-url)
A domain \( V \) is divided into linear tetrahedral finite elements connected at nodes as shown in figure A1. Shape functions \( N_i \) are used for interpolation of concentration inside a finite element,

\[
C = [N][C]
\]

where

\[
[N] = [N_1 \ N_2 \ N_3 \ N_4]
\]

\[
\{C\} = \begin{bmatrix} C_1 \\ C_2 \\ C_3 \\ C_4 \end{bmatrix}
\]

Here \( \{C\} \) is a vector of concentrations at nodes and \([N]\) is a matrix of shape functions. Using the Galerkin method, we can write equation (A1) in the following form:

\[
\int_V N_i \frac{\partial C}{\partial t} - D \left( \frac{\partial}{\partial x} \left( \frac{\partial C}{\partial x} \right) + \frac{\partial}{\partial y} \left( \frac{\partial C}{\partial y} \right) + \frac{\partial}{\partial z} \left( \frac{\partial C}{\partial z} \right) \right) dV = 0
\]

(A2)

Applying the divergence theorem to the terms in the bracket \( \{\} \), we arrive at the relations:

\[
\int_V N_i \frac{\partial C}{\partial t} dV + \int_D \left( \frac{\partial N_i}{\partial x} \frac{\partial C}{\partial x} + \frac{\partial N_i}{\partial y} \frac{\partial C}{\partial y} + \frac{\partial N_i}{\partial z} \frac{\partial C}{\partial z} \right) dV
\]

\[
- D \int_S \left[ N_i \frac{\partial C}{\partial n_x} n_x + N_i \frac{\partial C}{\partial n_y} n_y + N_i \frac{\partial C}{\partial n_z} n_z \right] dS = 0
\]

(A3)

where \( n_x \), \( n_y \), and \( n_z \) are outer normal components to the surface of the body. Since we applied the zero flux boundary condition at the surface of the body, the last terms in the integral of \( S \) is zero. Now the equation (A3) can be simplified as,

\[
\left( \int_V [N][N] dV \right) \left( \frac{dC}{dt} \right) + D \left( \int_V \left[ \frac{\partial N_i}{\partial x} \right] \left[ \frac{\partial N_i}{\partial x} \right] dV + \int_V \left[ \frac{\partial N_i}{\partial y} \right] \left[ \frac{\partial N_i}{\partial y} \right] dV + \int_V \left[ \frac{\partial N_i}{\partial z} \right] \left[ \frac{\partial N_i}{\partial z} \right] dV \right) [C] = 0
\]

Let's denote

\[
[K_c] = \int_V [N][N] dV
\]

\[
[K_D] = \int_V \left[ \frac{\partial N_i}{\partial x} \right] \left[ \frac{\partial N_i}{\partial x} \right] dV + \int_V \left[ \frac{\partial N_i}{\partial y} \right] \left[ \frac{\partial N_i}{\partial y} \right] dV + \int_V \left[ \frac{\partial N_i}{\partial z} \right] \left[ \frac{\partial N_i}{\partial z} \right] dV
\]

The discretized finite element equation for the mass transport equation can be rewritten as in equation (3),

\[
[K_c] \left( \frac{dC}{dt} \right) + D[K_D][C] = 0
\]

(A4)
References